

# On the Size Reduction of Slotted Finite Ground Plane of a Circularly Polarized Microstrip Patch Antenna Using Substructure Characteristic Modes

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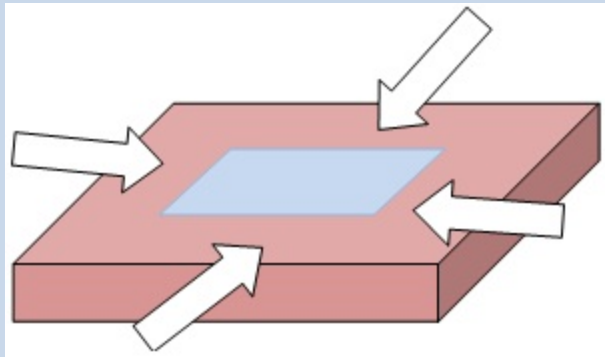
Paper id : 1570499018

# Outline of the Presentation

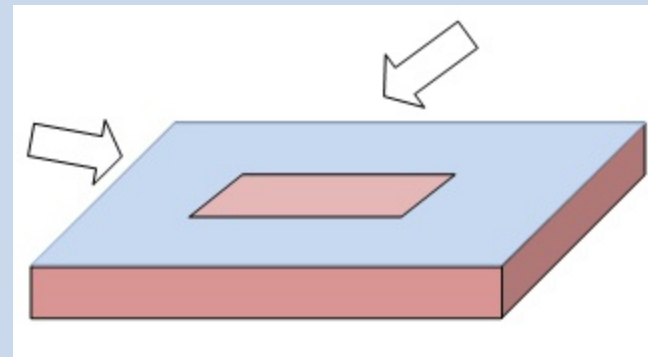
- Introduction
- The Problem in Hand
- Solution Technique
- Antenna Design
- CM Analysis
- Simulation Results
- Discussions
- Future Works

# Introduction

- Slotted ground/ defected ground helps decreasing the resonant frequency of a microstrip antenna
- Also miniaturization of the patch can be achieved by inserting slots on the ground
- Size reduction of the ground plane can be a challenge



Patch



Slotted ground

# The Problem in Hand

- Our question : How to reduce the ground plane (slotted) size at a particular frequency ?
- Aim is to reduce the overall size of the antenna
- Interest: To what extent we can reduce the overall antenna size keeping the frequency of operation same as well as achieving circular polarization.
- We investigate this using substructure based TCM
- The proposed technique can compute the modes of each object separately in a whole system

# Solution Technique: Substructure TCM of Substrate Based Patch Antenna

- Substructure based TCM [1] is required to accurately characterize the CMs of the metallic parts of the antenna in dielectric environment
- It gives CMs of metallic patch and ground plane separately

$$\begin{bmatrix} Z_{d,d} & Z_{d,cdp} & Z_{d,cdg} & Y_{d,d} & Z_{d,cp} & Z_{d,cg} \\ Z_{cdp,d} & Z_{cdp,cdp} & Z_{cdp,cdg} & Y_{cdp,d} & 0 & 0 \\ Z_{cdg,d} & Z_{cdg,cdp} & Z_{cdg,cdg} & Y_{cdg,d} & 0 & 0 \\ Y_{d,d} & Y_{d,cdp} & Y_{d,cdg} & Z_{d,d} & Y_{d,cp} & Y_{d,cg} \\ Z_{cp,d} & 0 & 0 & Y_{cp,d} & Z_{cp,cp} & Z_{cp,cg} \\ Z_{cg,d} & 0 & 0 & Y_{cg,d} & Z_{cg,cp} & Z_{cg,cg} \end{bmatrix} \begin{bmatrix} I_d \\ I_{cdp} \\ I_{cdg} \\ m_d \\ I_{cp} \\ I_{cg} \end{bmatrix} = \begin{bmatrix} V_a \\ V_b \\ V_c \\ i \\ V_e \\ V_f \end{bmatrix} \dots(1)$$

Replacing other variables for  $I_{cp}$  and  $I_{cg}$  taking the right hand side zero

For the patch  $[Z_p][I_{cp}] = [V_p] \dots(2)$  where,  $[Z_p] = [R_p] + j[X_p]$

For the ground  $[Z_g][I_{cg}] = [V_g] \dots(3)$  where,  $[Z_g] = [R_g] + j[X_g]$

[1] J. L. T. Ethier and D. A. McNamara, "Sub-structure characteristic mode concept for antenna shape synthesis," in *Electronics Letters*, vol. 48, no. 9, pp. 471-472, 26 April 2012.

[2] A. Kishk and L. Shafai, "Different formulations for numerical solution of single or multibodies of revolution with mixed boundary conditions," in *IEEE Transactions on Antennas and Propagation*, vol. 34, no. 5, pp. 666-673, May 1986.

# Solution Technique

The Generalized eigenvalue problem is constructed as follows

$$\text{For the patch } [\mathbf{X}_p][\mathbf{I}_n^{\text{cp}}] = \lambda_n^c[\mathbf{R}_p][\mathbf{I}_n^{\text{cp}}] \dots (4)$$

$$\text{For the ground } [\mathbf{X}_g][\mathbf{I}_n^{\text{cg}}] = \lambda_n^g[\mathbf{R}_g][\mathbf{I}_n^{\text{cg}}] \dots (5)$$

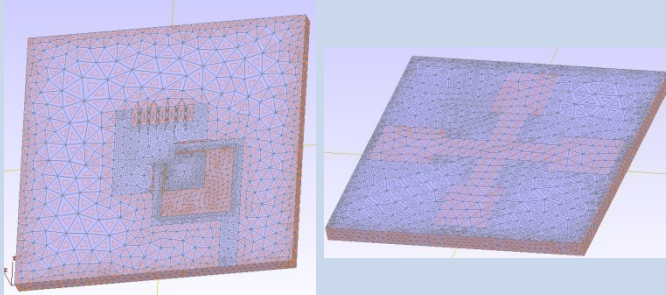
The CM currents on the patch and the ground plane in (6) and (7) respectively

$$\mathbf{J}_n^{\text{cp}} = \sum_m \mathbf{f}_m^p I_{n,m}^{\text{cp}} \dots (6)$$

$$\mathbf{J}_n^{\text{cg}} = \sum_m \mathbf{f}_m^g I_{n,m}^{\text{cg}} \dots (7)$$

# Antenna Design

- The substructure technique is used here to address the present problem
- Substructure modes helps in obtaining this loading effect separately in a strong mutual coupling environment
- In order to study, Microstrip patch antenna with cross slot loaded ground plane is simulated in EMCoS Antenna VLab using plane wave excitation
- EMCoS uses a special Greens' function and gives only conductor currents for finite substrate operation
- Slot on ground plane loads the patch and helps miniaturizing it
- Cross slot controls both modal currents to obtain CP
- The patch also loads the ground plane to reduce resonant frequency

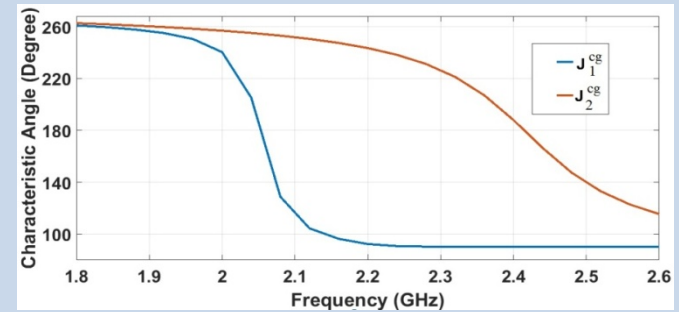
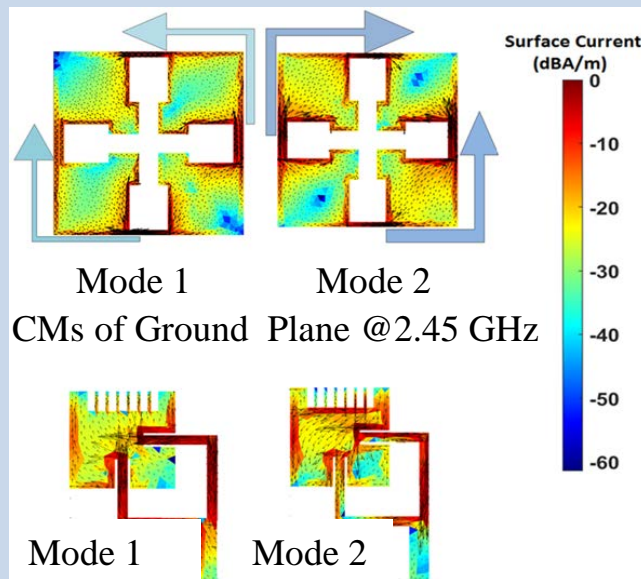


Meshed structure in EMCoS

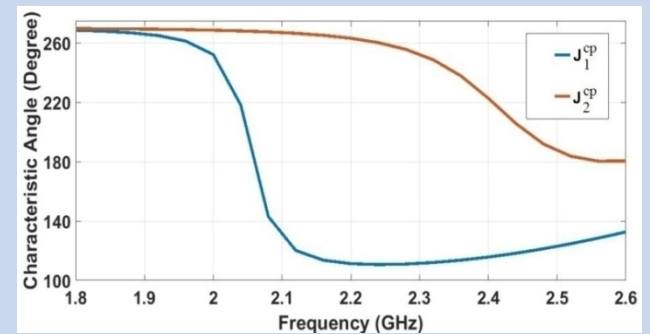
- The meshed structure is shown here, by varying iteratively (experiment) the size of the ground plane, ground slot and the patch, we obtain desired operation
- Loading effect between patch and ground plane needs to be studied in order to reduce overall size

# CM Analysis

- MoM matrix is extracted from EMCoS
- In-house MATLAB code is developed to evaluate eigenvalues and eigencurrents of the patch and ground plane separately
- Eigencurrent tracking method is used to track the modes over the whole frequency range of interest



CA plot of the ground plane

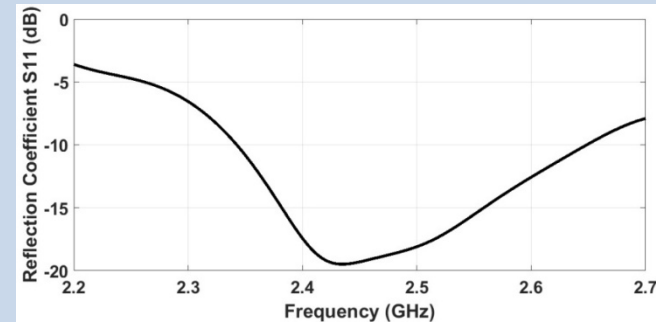
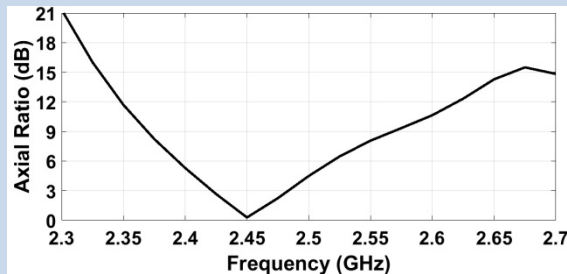
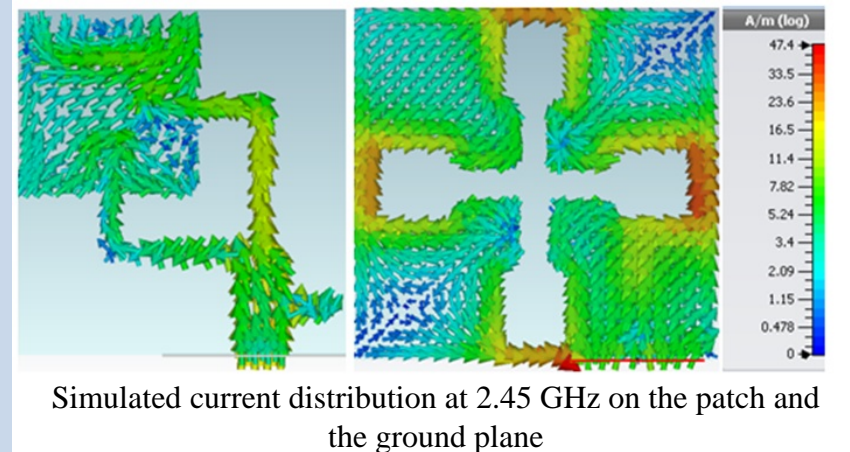
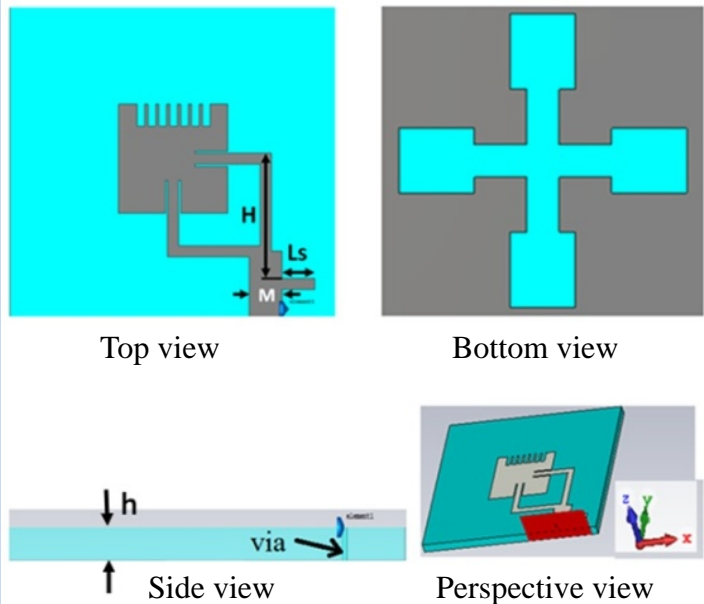


CA plot of the patch

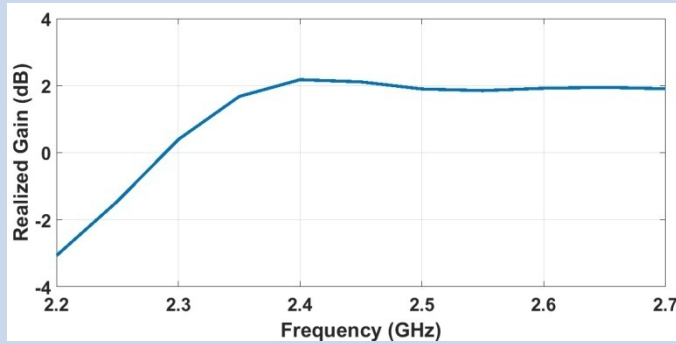
- The teeth on the top edge of the patch are introduced to adjust the eigenvalue curve so that the desired CP operation of the antenna is obtained



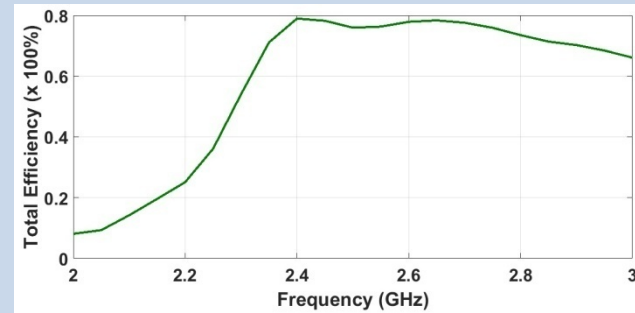
# Simulation Results



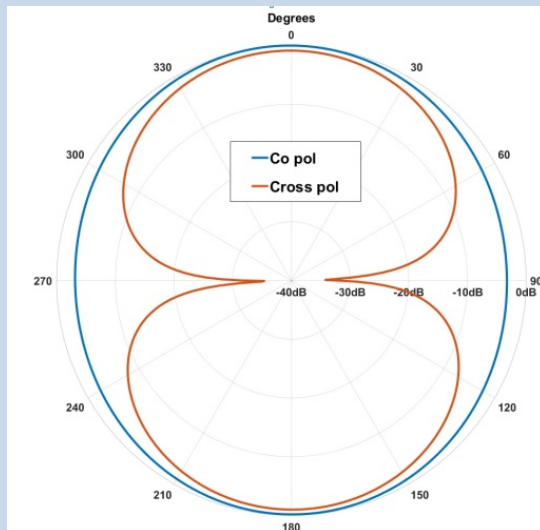
# Simulation Results



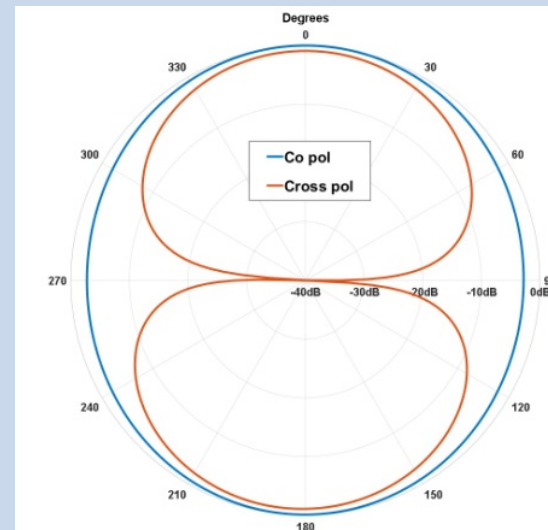
Realized gain plot



Total efficiency plot



Normalized pattern at 2.45 GHz on x-z plane  
(phi=0 degree)



Normalized pattern at 2.45 GHz on y-z plane  
(phi=90 degree)

# Discussions

- The overall antenna size is  $0.246\lambda_0 \times 0.237\lambda_0$ . The area of the ground plane is reduced by 56% as compared to half wave patch at the same frequency. The size of the patch is reduced by 94%
- 7542 RWG bases with an average execution time of 1minute for each frequency point (intel Xeon @3.30GHz, 32 GB memory size) but using special Greens' function it takes only 3 seconds for each point
- A low profile miniaturized antenna is obtained by using this technique
- The patch is used to miniaturize the ground plane size further
- The radiation pattern becomes bidirectional as the ground plane is having a cross slot on it
- It can be used as a repeater antenna in cars

# Future Works

- The antenna can be mounted on a suitable platform to get unidirectional radiation pattern
- The theory of substructure modes is applicable to ---
  - Multilayer antennas
  - Antennas on complex platform
  - Antenna in devices

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